(19) World Intellectual Property Organization International Bureau





(43) International Publication Date 12 December 2002 (12.12.2002)

PCT

(10) International Publication Number WO 02/098502 A2

(51) International Patent Classification⁷:

A61N 1/00

(21) International Application Number: PCT/US02/17393

(22) International Filing Date: 31 May 2002 (31.05.2002)

(25) Filing Language:

English

(26) Publication Language:

English

(30) Priority Data:

09/872,956

1 June 2001 (01.06.2001) U

- (71) Applicant: BIOFISICA, LLC [US/US]; 1961 Travers Circle, Lawrenceville, GA 30044 (US).
- (72) Inventors: ANDINO, Rafael; 1961 Travers Circle, Lawrenceville, GA 30044 (US). BROOKS, Christopher; 13 Meadow Lane, Glen Head, NY 11545 (US). VAN, Royen, Donald; 284 West End Avenue, Apartment 4B, New York, NY 10023 (US).
- (74) Agents: JACKSON, Robert, R. et al.; Fish & Neave, 1251 Avenue of the Americas, New York, NY 10020 (US).
- (81) Designated States (national): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CO, CR, CU,

CZ, DE, DK, DM, DZ, EC, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, MZ, NO, NZ, OM, PH, PL, PT, RO, RU, SD, SE, SG, SI, SK, SL, TJ, TM, TN, TR, TT, TZ, UA, UG, UZ, VN, YU, ZA, ZM, ZW.

(84) Designated States (regional): ARIPO patent (GH, GM, KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE, TR), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

Declarations under Rule 4.17:

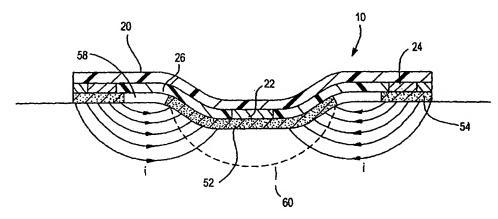
- as to applicant's entitlement to apply for and be granted a patent (Rule 4.17(ii)) for all designations
- as to the applicant's entitlement to claim the priority of the earlier application (Rule 4.17(iii)) for all designations

Published:

 without international search report and to be republished upon receipt of that report

For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

(54) Title: APPARATUS AND METHODS FOR FACILITATING WOUND HEALING



(57) Abstract: An electrode system is provided that generates a current flow that envelops and permeates an entire wound site. The electrode system includes two electrodes that are shaped and oriented to cause the current to flow from one electrode through the wound to the other electrode. A first electrode is applied to the wound site and the second electrode encircles the first electrode and is applied to the skin surrounding the wound cite. The two electrodes may be mounted to an oxygen-permeable layer that provides support for the electrodes and allows the wound site to breathe. An electrically insulative element may be disposed between the two electrodes. A power supply, which may be local to or remote from the electrode system, is provided for applying a voltage potential across the electrodes. In another suitable embodiment, the two electrodes are comprised of oppositely charged polymers.

7O 02/098502 A2

BEST AVAILABLE COPY

APPARATUS AND METHODS FOR FACILITATING WOUND HEALING

[0001] The present invention relates generally to apparatus and methods for facilitating wound healing through the use of electrical stimulation, and more particularly to apparatus and methods for providing a voltage gradient and a pattern of current flow that envelopes and permeates the wound.

10 Background of the Invention

- [0002] Connective tissue wound healing typically occurs in three distinct phases. Although these phases intertwine and overlap, each has a specific sequence of events that distinguishes it. During the initial, or
- inflammatory phase, the body begins to clean away bacteria and initiate hemostasis. The inflammatory phase has three subphases: hemostasis; leukocyte and macrophage migration; and epithelialization. This phase typically lasts for about four days.
- 20 [0003] The second phase, the proliferative phase, is characterized by a proliferation of fibroblasts, collagen synthesis, granulation, and wound contraction. The proliferative phase typically begins about 48 hours after the wound is inflicted and can extend anywhere
- 25 from two hours up to a week. In this phase, the

. - 2 -

fibroblast cells begin the synthesis and deposition of the protein collagen, which will form the main structural matrix for the successful healing of the wound.

5 [0004] In the third phase, the remodeling phase, the collagen production slows. The collagen that is formed in this stage is more highly organized than the collagen formed in the proliferative phase.

Eventually, the remodeled collagen increases the

10 tensile strength in the wound and returns the wound to about 80% of the skin's original strength.

[0005] This is the general process that occurs in healthy human beings. Patients that suffer from conditions which limit the flow of blood to the wound

site are unfortunately not able to exhibit the normal wound healing process as described. In some patients this process can be halted. Factors that can negatively affect this normal wound healing process include diabetes, impaired circulation, infection,

20 malnutrition, medication, and reduced mobility. Other factors such as traumatic injuries and burns can also impair the natural wound healing process.

[0006] Poor circulation, for varying reasons, is the primary cause of chronic wounds such as venous stasis ulcers, diabetic ulcers, and decubitus foot ulcers.

Venous stasis ulcers typically form just above the patient's ankles. The blood flow in this region of the legs in elderly or incapacitated patients can be very sluggish, leading to drying skin cells. These skin

30 cells are thus oxygen starved and poisoned by their own waste products and begin to die. As they do so, they leave behind an open leg wound with an extremely poor chance of healing on its own. Diabetic foot ulcers

form below the ankle, in regions of the foot that have very low levels of circulation.

Similarly, decubitus ulcers form when skin is [0007] subjected to constant compressive force without

- 5 movement to allow for blood flow. The lack of blood flow leads to the same degenerative process as described above. Paraplegics and severely immobile elderly patients which lack the ability to toss and turn while in bed are the main candidates for this 10 problem.
 - Traditional approaches to the care and [8000] management of these types of chronic non-healing wounds have included passive techniques that attempt to increase the rate of repair and decrease the rate of
- 15 tissue destruction. Examples of these techniques include antibiotics, protective wound dressings, removal of mechanical stresses from the affected areas, and the use of various debridement techniques or agents to remove wound exudate and necrotic tissue.
- For the most part, these treatment approaches 20 [0009] are not very successful. The ulcers can take many months to heal and in some cases they may never heal or they may partially heal only to recur at some later time.
- Active approaches have been employed to 25 [0010] decrease the healing time and increase the healing rates of these ulcers. These approaches may include surgical treatment as well as alterations to the wound environment. These alterations may include the
- 30 application of a skin substitute impregnated with specific growth factors or other agents, the use of hyperbaric oxygen treatments, or the use of electrical stimulation. It has also been shown experimentally

- 4 -

(both in animal and clinical trials) that specific types of electrical stimulation will alter the wound environment in a positive way so that the normal wound healing process can occur or in some cases occur in an accelerated fashion.

[0011] Therapeutic Electrostimulation

The relationship between direct current [0012] electricity and cellular mitosis and cellular growth has become better understood during the latter half of 10 the twentieth century. Weiss, in Weiss, Daryl S., et. al., Electrical Stimulation and Wound Healing, Arch Dermatology, 126:222 (Feb. 1990), points out that living tissues naturally possess direct current electropotentials that regulate, at least in part, the 15 wound healing process. Following tissue damage, a current of injury is generated that is thought to trigger biological repair. This current of injury has been extensively documented in scientific studies. It is believed that this current of injury is instrumental 20 in ensuring that the necessary cells are drawn to the wound location at the appropriate times during the various stages of wound healing. Localized exposure to low levels of electrical current that mimic this naturally occurring current of injury has been shown to 25 enhance the healing of soft tissue wounds in both human subjects and animals. It is thought that these externally applied fields enhance, augment, or take the place of the naturally occurring biological field in the wound environment, thus fostering the wound healing 30 process.

[0013] Weiss continues to explain, in a summary of the scientific literature, that intractable ulcers have demonstrated accelerated healing and skin wounds have resurfaced faster and with better tensile properties
5 following exposure to electrical currents. Dayton and Palladino, in Dayton, Paul D., and Palladino, Steven J., Electrical Stimulation of Cutaneous Ulcerations — A Literature Review, Journal of the American Podiatric Medical Association, 79(7):318 (July 1989), also state
10 that the alteration of cellular activity with externally applied currents can positively or negatively influence the status of a healing tissue, thereby directing the healing process to a desired outcome.

- Furthermore, research conducted by Rafael 15 [0014] Andino during his graduate tenure at the University of Alabama at Birmingham, also demonstrated that the presence of electrical fields (in this case induced by the application of pulsating electromagnetic fields) 20 dramatically accelerated the healing rates of wounds created in an animal model. This research found that the onset and duration of the first two phases of the wound healing process, the inflammatory and proliferative phases, had been markedly accelerated in 25 the treated wounds while the volume of collagen which had been synthesized by the fibroblasts was also markedly increased in the treated wounds. resulted in the wounds healing in a much shorter amount of time. Similar findings from other researchers can 30 be found in other wound healing literature.
 - [0015] U.S. Pat. No. 5,433,735 to Zanakis et al. and U.S. Pat. No. 4,982,742 to Claude describe various electro-stimulation apparatus and techniques for

facilitating the regeneration and repair of damaged tissue. However, each of these references suffers from the disadvantage that the pattern of current flow generated with these electrode devices does not pass 5 through all portions of the wound and thus, certain portions of the wound site may not be exposed to the beneficial effects of electrostimulation. U.S. Pat. No. 4,911,688 to Jones describes a wound cover that includes a chamber that encloses fluid 10 around the wound. One electrode is located in the chamber and another electrode is placed away from the wound on the skin. By using conductive liquid within the chamber, a circuit is completed allowing current to flow from the electrode in the chamber, through the 15 liquid, wound, and surrounding tissue and skin to the other electrode. The liquid is introduced into the chamber and replaced using two ports, one port is used to introduce the liquid while at the same time the other port is used to remove the gas (when the wound 20 cover is originally applied to the wound) or fluid within the chamber. This wound cover, however, is complicated to use and involves a delicate process of adding and replacing the conductive liquid. In view of the foregoing, it is an object of [0017] 25 the present invention to provide improved apparatus and methods for easily providing a voltage gradient and a pattern of current flow that envelops and permeates the

Summary of the Invention

entire wound site.

30 [0018] This and other objects of the invention are accomplished in accordance with the principles of the present invention by providing an electrode system that

- 7 -

includes two electrodes that are adapted for connection to a power source sufficient to cause a current to flow between them. The electrodes are shaped and oriented to cause a pattern of current flow that envelops and 5 permeates the entire wound site. Such shapes and orientations may include a circular first electrode located at and covering the wound site and a second electrode shaped as a ring fully encircling the first electrode. The second electrode may be located outside 10 or partially within the wound site. Other suitable shapes of the electrodes may include electrodes that are ovally shaped, rectangularly shaped, triangularly shaped or any other suitable shape where one electrode encircles the other electrode. The shape of the 15 electrode may conform to the shape of the wound. The two electrodes of the electrode system [0019] may be mounted to an oxygen-permeable top layer that is impermeable to water and water vapor. The top layer may provide support for the electrodes and may allow 20 the wound site to breathe.

[0020] The electrode system may also include an electrically insulative element that is disposed between the two electrodes. The insulative element may ensure that most if not all of the current flow between the electrodes passes through the damaged and healthy surrounding tissue.

[0021] The power supply for applying a voltage potential across the electrodes may be local to or remote from the electrode system. In one suitable arrangement, the power supply is attached to the top layer of the electrode system. The power supply can be configured to provide a constant or varying voltage, a constant or varying current, or any other suitable

electrical output to the electrodes to facilitate wound healing. For example, the power supply may be configured to provide the desired current or voltage to the electrodes at different time intervals with the same electrode system in place. In one suitable embodiment, the power supply is a battery. In another suitable embodiment, the power supply is electronic circuitry that is configured to provide the desired current or voltage.

10 [0022] In another suitable embodiment of the invention, the two electrodes of the electrode system are comprised of oppositely charged polymers of sufficient voltage differential and charge capacity to cause a current to flow from the first electrode to the second electrode through the wound.

[0023] The electrode system can be designed and fabricated to be either disposable or reusable.

[0024] The electrode system according to the various embodiments described herein is capable of generating a voltage gradient and a pattern of current flow that envelops and permeates the entire wound site. Such a pattern of current flow maximizes the recruitment of

appropriate times during the various stages of wound 25 healing.

the necessary cells to the wound location at the

Brief Description of the Drawings

[0025] The above and other objects and advantages of the invention will be apparent upon consideration of the following detailed description, taken in conjunction with the accompanying drawings, in which like reference characters refer to like parts throughout, and in which:

[0026] FIG. 1 is a cross-sectional view of an illustrative electrode system in accordance with the present invention taken generally along the line 1-1 of .FIG. 2.

5 [0027] FIG. 2 is a cross-sectional view of the electrode system of FIG. 1 taken generally along the line 2-2 of FIG. 1

[0028] FIG. 3 is a cross-sectional view of the electrode system of FIG. 1 as applied to a wound that

10 illustrates the pattern of current flow generated by the electrode system in accordance the present invention.

[0029] FIG. 4 is a perspective view of an illustrative electrode system placed over a wound site in accordance with the present invention.

Detailed Description of the Preferred Embodiments

[0030] FIG. 1 is a cross-sectional view of electrode system 10. The view in FIG. 1 is taken along the line 1-1 of FIG. 2. FIG. 2 shows a simplified cross-

- sectional view of electrode system 10 taken alone the line 2-2 of FIG. 1. As illustrated in FIG. 1, electrode system 10 includes top overlay layer 20 to which electrodes 22 and 24, electrically insulative element 26, and end material 28 are attached.
- 25 Electrode 22 is located towards the center of top overlay layer 20. Electrically insulative element 26 surrounds electrode 22 and electrode 24 surrounds electrically insulative element 26. Attached to the other side of electrodes 22 and 24, electrically
- insulative element 26, and end material 28 are adhesive layers 52 and 54. As illustrated in FIG. 2, electrically conductive lead 32 connects electrode 22

WO 02/098502

PCT/US02/17393

to terminal 42 of power supply 40 and electrically conductive lead 34 connects electrode 24 to terminal 44 of the power supply 40.

[0031] Top overlay layer 20 may serve several

5 different purposes. First, top overlay layer 20
provides the mechanical integrity of electrode system
10, thus providing structural support for electrodes 22
and 24. Second, top overlay layer 20 should be
flexible enough to allow electrode system 10 to conform

- 10 to the contours of the skin surface to which it is adhered. Third, top overlay layer 20 should be oxygen permeable to allow the wound site to breathe. Finally, top overlay layer 20 should be water impermeable so that the wound site remains moist. In some
- embodiments, all of these characteristics may not be necessary. For example, a separate water impermeable layer may be used to keep the wound site moist. Top overlay layer 20 may be comprised of any suitable material or structure that exhibits these
- 20 characteristics. For example, top overlay layer 20 may be comprised of a mesh structure of polypropylene, polyethylene, polyurethane, polytetrafluoroethylene (PTFE), or any other suitable material. In one embodiment, top overlay layer 20 can be electrically
- 25 insulative to prevent current from flowing between electrodes 22 and 24, which are attached to top overlay layer 20. In another suitable embodiment, the adhesive or binding agent (not shown) used to adhere electrodes 22 and 24 to top overlay layer 20 can be electrically
- 30 insulative to prevent current from flowing between electrodes 22 and 24.

[0032] Electrodes 22 and 24 may be thin metal, metallic paint or pigment deposition, metallic foil,

conductive hydrogels, or any other suitable conductive material. Hydrogels are generally clear, viscous gels that protect the wound from dessicating. suitable approach, conductive hydrogels may be used as 5 the material for electrodes 22 and 24 because of their permeability to oxygen and ability to retain water. Both oxygen and a humid environment is required for the cells in a wound to be viable. In addition, hydrogels can be easily cast into any shape and size. Various 10 types of conductive hydrogels may be employed, including cellulose, gelatin, polyacrylamide, polymethacrylamide, poly(ethylene-co-vinyl acetate), poly(N-vinyl pyrrolidone), poly(vinyl alcohol), HEMA, HEEMA, HDEEMA, MEMA, MEEMA, MDEEMA, EGDMA, mathacrylic acid based materials, and siliconized hydrogels. PVAbased hydrogels are inexpensive and easy to form. The conductivity of such hydrogels can be changed by varying the salt concentration within the hydrogels. By increasing the salt concentration within a hydrogel, 20 the conductivity of the hydrogel increases. Insulative element 26 prevents the flow of current between electrodes 22 and 24 above the wound surface such as by moisture trapped under the top overlay layer. Insulative element 26 may be composed 25 of any high resistance material such as polythylene, poly(tetrafluoroethylene) (TEFLON), polyurethane, polyester, a hydrogel made to be an insulator or any other suitable insulative material. In addition, insulative element 26 may be formed of a material or 30 designed to have gaps or openings within its body to prevent the flow of current or greatly increase the current resistance above the wound surface.

End material 28 surrounds electrode 24. End [0034] material 28, in combination with the outer edge of top overlay layer 20, forms the outer edge of electrode system 10. End material 28 may be comprised of any 5 suitable material flexible enough to allow electrode system 10 to conform to the contours of the skin surface to which it is adhered. In one embodiment, end material 28 may be composed of the same material as top overlay layer 20. In one suitable approach, end 10 material 28 may be a part of and seamless with top overlay layer 20. Conductive adhesive layers 52 and 54 are [0035] attached to the underside of electrode system 10, contacting electrodes 22 and 24, respectively and 15 electrically insulative element 26. Adhesive layers 52 and 54 should be separated from each other by a suitable space or gap 58 to prevent short-circuiting of the electrodes. Adhesive layers 52 and 54 may be a hydrogel, fibrin, conductively transformed 20 cyanoacrylates or can be comprised of any suitable electrically conductive material capable of attaching electrode system 10 to the skin and wound surfaces. Adhesive layer 52 can be arranged to distribute substantially the same voltage of electrode 22 to the 25 entire surface of the wound. Similarly, adhesive layer 54 can be arranged to distribute substantially the same voltage of electrode 24 to the skin surrounding the In another suitable approach, adhesive layer 52 can be arranged so that the center of adhesive layer 52 30 applies a voltage substantially similar to electrode 22 to the center of the wound and that the outer edge of adhesive layer 52 applies a voltage that is between the

voltages of electrodes 52 and 54 to the outer edge of

the wound. The voltage applied to the wound may be varied, for example, by varying the thickness of adhesive 52 or by any other suitable method.

[0036] As illustrated in FIG. 1, adhesive layer 52 extends beyond electrode 22. In another suitable arrangement, adhesive layer 52 may be the same size as or smaller than electrode 22. Adhesive layer 54 as illustrated is larger than electrode 24. In another suitable arrangement, adhesive layer 54 may be the same size as or smaller than electrode 24.

[0037] In another suitable embodiment, conductive adhesive layers 52 and 54 may be omitted from electrode system 10. In this embodiment, electrodes 22 and 24 are themselves adhesive and capable of attaching

- electrode system 10 to the wound site. Conductive hydrogels can be fashioned to have the requisite adhesive properties, thereby eliminating the need for separate adhesive layers. One type of highly conductive hydrogel that is sufficiently tacky and
- 20 adhesive to adhere to the skin is described in U.S.
 Pat. No. 4,989,607 to Keusch et al. Electrodes 22 and
 24 may be comprised of any suitable conductive adhesive
 material capable of attaching electrode system 10 to
 the wound site.
- 25 [0038] Backing layer 60 is attached to conductive adhesives 52 and 54 to protect the adhesive layer prior to the use of electrode system 10. Backing layer 60 may be peeled off of adhesives 52 and 54 to expose the adhesive layer prior to contacting electrode system 10 to the wound site. Backing layer 60 may protrude out from underneath top overlay layer 20 in one area, such as area 60' as shown in FIG. 2, to allow the user to

PCT/US02/17393 WO 02/098502

- 14 -

easily remove backing layer 60 from electrode system 10.

In use, electrode system 10 is positioned 100391 over the wound site such that electrode 22 is located 5 at approximate the center of the wound site and adhesive layer 52 can be sized to cover the entire wound. Electrode system 10 is provided in a family of sizes appropriate for wounds of various sizes. Electrode 24 and adhesive layer 54 are generally in the 10 shape of a ring and are located a distance away from electrode 22. In one arrangement, the diameters of the inner edges of electrode 24 and adhesive layer 54 are greater than the diameter of the wound. In another words, the size of the wound determines the minimum 15 inner diameter of electrode 24 and adhesive layer 54. In another suitable arrangement, adhesive layer 52 can be sized to cover the inner portion of the wound and the inner diameters of the inner edges of electrode 24 and adhesive layer 54 may be the same or less than the size of the wound. 20

FIG. 3 is a cross-sectional view of electrode system 10 as applied to wound 60. As shown in FIG. 3, the pattern of current flow generated by electrode system 10 is toroidal in shape. A toroid is generally formed by rotating a circular disk about an axis, where the axis lies in the plane of the disk, but outside of the disk. Here, the pattern of current flow is similar to a semicircle rotated about an axis, where the axis lies in the plane of the semicircle and the axis is 30 near the edge of the semicircle. The current generally flows tangential to the radial lines of the semicircle. Because electrode 24 surrounds electrode 22, the pattern of current flow is similar to the semicircular

25

disk rotated completely around the axis. Therefore, the pattern of current flow is toroidal in shape. pattern of current flow as illustrated in FIG. 3 would therefore generally be the same regardless of the angle 5 of the cross-section cut through electrode system 10 with respect to reference direction 65 of Fig. 2. More specifically, as illustrated, electrode 22 is negatively charged and electrode 24 is positively charged. The lines of current flow extend from 10 adhesive 54 through wound 60 to adhesive 52 in an arcuate shape. The lines of current pass through the entire wound 60, thereby enveloping and permeating the entire wound and the adjoining unwounded tissue. If the voltage that is applied to the wound from adhesive 15 52 is varied, as described above, then the current density at different portions of wound 60 can be increased or decreased accordingly. Electrode system 10 can produce a current density within the wound that is generally between 1 $\mu A/cm^2$ and 10,000 $\mu A/cm^2$.

Depending on the size and nature of the wound, electrode system 10 may be configured to produce a current density within the wound that is less than of 1 $\mu A/cm^2$ or greater 10,000 $\mu A/cm^2$.

[0041] Referring to FIG. 2, conductive leads 32 and 34, which connect electrodes 22 and 24 respectively to power supply 40, may be comprised of metal, conductive ink or any other suitable conductive material. In one suitable arrangement, leads 32 and 34 are comprised of conductive carbon ink that is screened onto top overlay layer 20. In such an arrangement, electrodes 22 and 24 are formed in place over conductive leads 32 and 34, respectively.

[0042] Power supply 40 generates a voltage that is applied to electrodes 22 and 24 through leads 32 and 34, respectively. Power supply 40 may be configured to apply a voltage that is anywhere between 1 mV and 9 V.

- 5 The resulting current flow that flows through the wound may be between 1 µA and 50 mA. Depending on the size and nature of the wound, power supply 40 may be configured to apply a voltage that is less than 1 mV or greater than 9 V. The resulting current flow may
- 10 therefore be less than 1 μA or greater than 50 mA.

 Power supply 40 may be attached to the upper portion of top overlay layer 20 or any other suitable location on electrode system 10 or may be located remote from electrode system 10. In one suitable embodiment, power
- 15 supply 40 is a battery. Power supply 40 may be any suitable battery such as an alkaline, nickel cadmium, or lithium battery. In one suitable arrangement, power supply 40 is a lithium polymer stack. The battery may be arranged so that terminal 42 is negative and
- terminal 44 is positive. Thus, electrode 22 functions as an anode and electrode 24 functions as a cathode.

 As described above, current will flow along outward radial lines from electrode 24 through the wound to electrode 22. In another suitable approach, the
- 25 battery can be arranged so that terminal 42 is positive and terminal 44 in negative. In such an approach, the lines of current are reversed and directed outward from electrode 22 to electrode 24.

[0043] In another suitable embodiment, power supply
30 40 is comprised of electronic circuitry that is
configured to provide a constant or varying voltage, a
constant or varying current, or any other suitable
electrical output. The current density within the

wound site may therefore be constant or time varying. When power supply 40 varies the voltage or current, electrodes 22 and 24 may change polarities at a constant or at a time varying frequency. In another suitable electrical output, power supply 40 can be configured to pulse electrodes 22 and 24 to provide other possible therapeutic benefits.

[0044] In one suitable arrangement, the electrical circuitry can be configured to provide a constant

- 10 current source using a current-to-voltage converter.

 The current to voltage converter may be probed at test points to check the current accuracy. The constant current source may be implemented with an operational amplifier (Op-amp). The Op-amp compares a precision
- voltage reference source to the output of a current-tovoltage converter and adjusts the output current until the reference and the converter are equal. The output voltage is limited to the battery voltage minus a certain predetermined amount used for operational
- [0045] The circuit may be built with surface mount integrated circuits and other surface mount components and may be powered, for example, by lithium coin cell

20 purposes.

batteries.

25 [0046] The electrode system 10 herein described may not require a switch to be activated for current to commence flowing between electrodes 22 and 24. Rather, current may begin to flow following conductive contact

of electrodes 22 and 24 to the wound site. Such

30 contact completes a circuit between the electrodes and results in current flow between the electrodes. In another suitable embodiment, a switch may be located on

WO 02/098502

PCT/US02/17393

electrode system 10 that may allow the user to engage and disengage power supply 40 to electrodes 22 and 24. Electrode system 10 may contain within its [00471 circuitry a visual indicator to allow the user to 5 determine whether or how well the electrode system is functioning. The visual indicator may be a light emitting diode (LED), a series of LEDs, a basic current meter, or any other suitable visual indicator. FIG. 4 demonstrates a view of electrode [0048] 10 system 10 placed over wound 60. In this embodiment, electrode system 10 is a disposable, one-time-use bandage that uses a battery and associated circuitry as power supply 40, which is attached to electrode system 10. Appropriate electrical parameters may be selected 15 such that the current generated by the internal circuitry will last for a desired period of time. example, the desired period of time may be at least as long as the typical amount of time a normal bandage is used on the wound. For users with chronic ulcers, this 20 amount of time may typically be 1 to 2 days. Therefore, after electrode system 10 is activated by placement over the wound, an electrical current may last for 1 to 2 days. When it is time for electrode system 10 to be replaced, a new electrode system will 25 be applied and the treatment will continue as required by the individual user and the type of wound present. While electrode system 10 has been described as being generally circular in shape, it is understood that electrode system 10 may also be provided in other 30 shapes as well. For example, electrode system 10 may be provided in an oval shape, rectangular shape, triangular shape, or any other suitable shape. The resulting pattern of current flow would therefore be

- 19 -

similar to the toroidal shape described above which has been stretch from a circle to an oval shape, rectangular shape, triangular shape, or any other suitable shape of electrode system 10. Electrode 5 system 10 is preferably provided in different shapes appropriate for wounds of different shapes. For example, if the wound is a long gash wound, a rectangular or oval shaped electrode system may be the appropriate shape for the wound. In one suitable 10 approach, a preferred electrode system shape for a wound is a shape that will allow adhesive 52 to cover the entire wound and that will minimize the amount of area that adhesive 52 covers exterior to the wound. This will maximize the current flow through the wound. In another suitable electrode system embodiment, electrodes 22 and 24 are electrically charged polymers. In this embodiment, power supply 40 and leads 32 and 34, as illustrated in FIGS. 1 and 2 are not required. In addition, top overlay layer 20 20 may not be required and electrodes 22 and 24 may be separately applied. Electrodes 22 and 24 can be oppositely charged polymers (e.g., hydrogel or any other suitable material for holding a charge) of sufficient differential voltage potential and of 25 sufficient charge densities to cause a current to flow between the electrodes. In one suitable arrangement, electrode 22 is negatively charged and electrode 24 is positively charged. This would cause current to flow through the wound to negative electrode 22 from 30 positive electrode 24. In another suitable arrangement, electrode 22 is positively charged and electrode 24 is negatively charged. This would cause current to flow from positive electrode 22 through the wound to negative electrode 24.

- 20 -

[0051] The foregoing is merely illustrative of the principles of this invention and various modifications can be made by those skilled in the art without departing from the scope and spirit of the invention.

PCT/US02/17393

WO 02/098502

- 21 -

WHAT IS CLAIMED IS:

- An electrode system for facilitating the healing of a wound, comprising:
 - a support structure;
- a first electrode attached to the support structure; and
- a second electrode attached to the support structure, wherein the second electrode surrounds the first electrode on the support structure, and wherein (a) when the electrode system is applied to the wound and (b) when a voltage potential is applied across the first and the second electrodes, a current is caused to flow between the first and the second electrodes, thereby passing through the wound.
- The electrode system defined in claim 1 2. further comprising an electrically insulative element attached to the support structure that is disposed between the first and the second electrodes.
- The electrode system defined in claim 1 3. further comprising a power source that is configured to apply the voltage potential across the first and the second electrodes.
- The electrode system defined in claim 3 wherein the power source is attached to the support structure.
- The electrode system defined in claim 3 wherein the power source is configured to apply a constant voltage potential across the first and the second electrodes.

- 6. The electrode system defined in claim 3 wherein the power source is configured to cause a constant current to flow between the first and the second electrodes.
- 7. The electrode system defined in claim 3 wherein the power source is configured to apply a time varying voltage potential across the first and the second electrodes.
- 8. The electrode system defined in claim 7 wherein the power source is configured to change the polarities of the first and the second electrodes when the time varying voltage potential is applied across the first and the second electrodes.
- 9. The electrode system defined in claim 1 wherein the current that is caused to flow between the first and the second electrodes causes a current density within the range of 1 $\mu A/cm^2$ to 10,000 $\mu A/cm^2$ to occur through the area of the wound.
- 10. The electrode system defined in claim 1 wherein the current is caused to flow from the first electrode through the wound to the second electrode.
- 11. The electrode system defined in claim 1 wherein the current is caused to flow from the second electrode through the wound to the first electrode.
- 12. The electrode system defined in claim 1 wherein the support structure is permeable to oxygen.

- 23 -

13. The electrode system defined in claim 1 wherein the support structure is impermeable to water and water vapor.

- 14. The electrode system defined in claim 1 further comprising a first adhesive material attached to the first electrode, wherein the first adhesive material attaches the first electrode to the wound when the electrode system is applied to the wound.
- 15. The electrode system defined in claim 1 further comprising a second adhesive material attached to the second electrode, wherein the second adhesive material attaches the second electrode to the skin surrounding the wound when the electrode system is applied to the wound.
- 16. The electrode system defined in claim 1 wherein the first electrode covers the entire wound when the electrode system is applied to the wound.
- 17. The electrode system defined in claim 1 wherein the first and the second electrodes are selected from the group consisting of thin metal, metallic deposition, metallic foil, and conductive hydrogels.
- 18. The electrode system defined in claim 1 further comprising a visual indicator to allow the user to determine whether or how well the electrode system is functioning.
- 19. An electrode system for facilitating the healing of a wound, comprising:

a first electrode that covers the entire wound when the first electrode is applied to the wound; and

a second electrode that surrounds the first electrode when the first and the second electrodes are applied to the wound, wherein (a) when the first and the second electrodes are applied to the wound and (b) when a voltage potential is applied across the first and the second electrodes, a current is caused to flow between the first and the second electrodes, thereby passing through the wound.

- 20. The electrode system defined in claim 19 further comprising an electrically insulative element that is disposed between the first and the second electrodes when the electrode system is applied to the wound.
- 21. The electrode system defined in claim 19 further comprising a power source that is configured to apply the voltage potential across the first and the second electrodes.
- 22. The electrode system defined in claim 21 wherein the power source is configured to apply a constant voltage potential across the first and the second electrodes.
- 23. The electrode system defined in claim 21 wherein the power source is configured to cause a constant current to flow between the first and the second electrodes.

- 25 -

- 24. The electrode system defined in claim 21 wherein the power source is configured to apply a time varying voltage potential across the first and the second electrodes.
- 25. The electrode system defined in claim 24 wherein the power source is configured to change the polarities of the first and the second electrodes when the time varying voltage potential is applied across the first and the second electrodes.
- 26. The electrode system defined in claim 19 wherein the current that is caused to flow between the first and the second electrodes causes a current density within the range of 1 $\mu A/cm^2$ to 10,000 $\mu A/cm^2$ to occur through the area of the wound.
- 27. The electrode system defined in claim 19 wherein the current is caused to flow from the first electrode through the wound to the second electrode.
- 28. The electrode system defined in claim 19 wherein the current is caused to flow from the second electrode through the wound to the first electrode.
- 29. The electrode system defined in claim 19 further comprising a first adhesive material attached to the first electrode, wherein the first adhesive material attaches the first electrode to the wound when the electrode system is applied to the wound.
- 30. The electrode system defined in claim 19 further comprising a second adhesive material attached to the second electrode, wherein the second adhesive

material attaches the second electrode to the skin surrounding the wound when the electrode system is applied to the wound.

- 31. The electrode system defined in claim 19 wherein the first and the second electrodes are selected from the group consisting of thin metal, metallic deposition, metallic foil, and conductive hydrogels.
- 32. The electrode system defined in claim 19 further comprising a visual indicator to allow the user to determine whether or how well the electrode system is functioning.
- 33. An electrode system for facilitating the healing of a wound, comprising:
 - a first electrode; and
- a second electrode, wherein the first and the second electrodes comprise oppositely charged polymers of sufficient differential voltage potential and sufficient charge densities to cause a current to flow from the first electrode to the second electrode through the wound when the electrode system is applied to the wound.
- 34. The electrode system defined in claim 33 further comprising a support structure to which the first and second electrode are attached.
- 35. The electrode system defined in claim 34 wherein the support structure is permeable to oxygen.

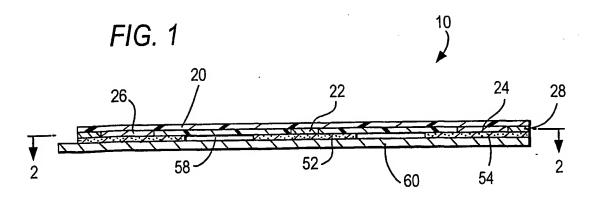
- 27 -

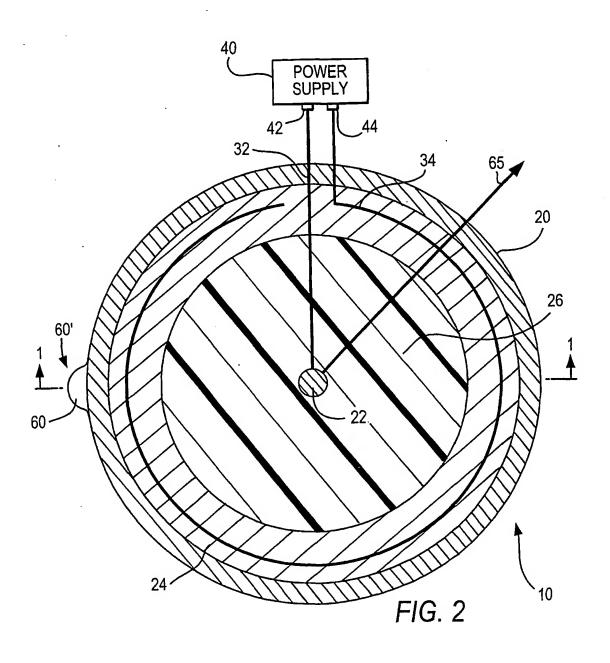
- 36. The electrode system defined in claim 34 wherein the support structure is impermeable to water and water vapor.
- 37. The electrode system defined in claim 34 wherein the second electrode surrounds the first electrode on the support structure.
- 38. The electrode system defined in claim 37 further comprising an electrically insulative element attached to the support structure that is disposed between the first and the second electrodes.
- 39. The electrode system defined in claim 34 wherein the first electrode surrounds the second electrode on the support structure.
- 40. The electrode system defined in claim 39 further comprising an electrically insulative element attached to the support structure that is disposed between the first and the second electrodes.
- 41. The electrode system defined in claim 33 wherein the current that is caused to flow between the first and the second electrodes causes a current density within the range of 1 $\mu A/cm^2$ to 10,000 $\mu A/cm^2$ to occur through the area of the wound.
- 42. The electrode system defined in claim 33 further comprising:
- a first adhesive material attached to the first electrode, wherein the first adhesive material attaches the first electrode to the wound when the electrode system is applied to the wound; and

- 28 -

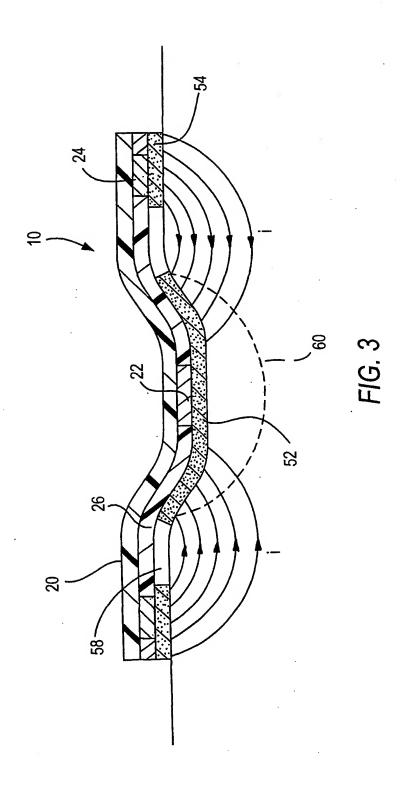
a second adhesive material attached to the second electrode, wherein the second adhesive material attaches the second electrode to the skin surrounding the wound when the electrode system is applied to the wound.

- 43. The electrode system defined in claim 42 wherein the first electrode covers the entire wound when the electrode system is applied to the wound.
- 44. The electrode system defined in claim 33 further comprising:
- a first adhesive material attached to the first electrode, wherein the first adhesive material attaches the first electrode to the skin surrounding the wound when the electrode system is applied to the wound; and
- a second adhesive material attached to the second electrode, wherein the second adhesive material attaches the second electrode to the wound when the electrode system is applied to the wound.
- 45. The electrode system defined in claim 44 wherein the second electrode covers the entire wound when the electrode system is applied to the wound.

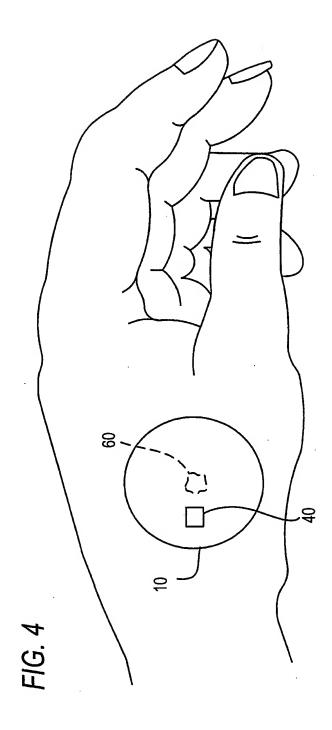




SUBSTITUTE SHEET (RULE 26)



SUBSTITUTE SHEET (RULE 26)



SUBSTITUTE SHEET (RULE 26)

(19) World Intellectual Property Organization International Bureau



1 DECEMBER 1 OF CONTRACT OF CO

(43) International Publication Date 12 December 2002 (12.12.2002)

PCT

(10) International Publication Number WO 02/098502 A3

- (51) International Patent Classification7: A61N 1/20, 1/32
- (21) International Application Number: PCT/US02/17393
- (22) International Filing Date: 31 May 2002 (31.05.2002)
- (25) Filing Language:

English

(26) Publication Language:

English

(30) Priority Data:

09/872,956

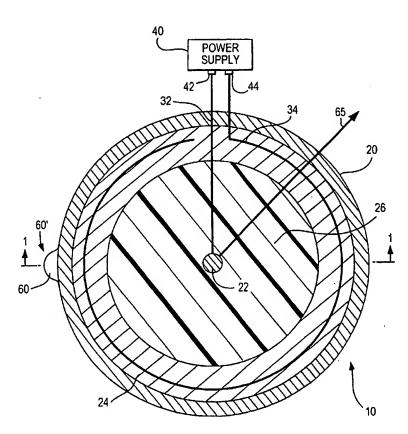
1 June 2001 (01.06.2001) US

- (71) Applicant: BIOFISICA, LLC [US/US]; 1961 Travers Circle, Lawrenceville, GA 30044 (US).
- (72) Inventors: ANDINO, Rafael; 1961 Travers Circle, Lawrenceville, GA 30044 (US). BROOKS, Christopher; 13 Meadow Lane, Glen Head, NY 11545 (US). VAN, Royen, Donald; 284 West End Avenue, Apartment 4B, New York, NY 10023 (US).

- (74) Agents: JACKSON, Robert, R. et al.; Fish & Neave, 1251 Avenue of the Americas, New York, NY 10020 (US).
- (81) Designated States (national): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, MZ, NO, NZ, OM, PH, PL, PT, RO, RU, SD, SE, SG, SI, SK, SL, TJ, TM, TN, TR, TT, TZ, UA, UG, UZ, VN, YU, ZA, ZM, ZW.
- (84) Designated States (regional): ARIPO patent (GH, GM, KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE, TR), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

[Continued on next page]

(54) Title: APPARATUS AND METHODS FOR FACILITATING WOUND HEALING



(57) Abstract: An electrode system (10) is provided that generates a current flow that envelops and permeates an entire wound site. The electrode system includes two electrodes (22,24) that are shaped and oriented to cause the current to flow from one electrode through the wound to the other electrode. A first electrode (22) is applied to the wound site and the second electrode (24) encircles the first electrode and is applied to the skin surrounding the wound cite. The two electrodes may be mounted to an oxygen-permeable layer that provides support for the electrodes and allows the wound site to breathe. An electrically insulative element (26) may be disposed between the two electrodes. A power supply (40), which may be local to or remote from the electrode system, is provided for applying a voltage potential across the electrodes. In another suitable embodiment, the two electrodes are comprised of oppositely charged polymers.

WO 02/098502 A3



Declarations under Rule 4.17:

- as to applicant's entitlement to apply for and be granted a patent (Rule 4.17(ii)) for all designations
- as to the applicant's entitlement to claim the priority of the earlier application (Rule 4.17(iii)) for all designations

Published:

- with international search report
- (88) Date of publication of the international search report:

30 October 2003

For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

INTERNATIONAL SEARCH REPORT

al Application No PCT7US 02/17393

A. CLASSIFICATION OF SUBJECT MATTER IPC 7 A61N1/20 A61N1/32

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols) IPC 7 $\,$ A61N $\,$

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, WPI Data

	Citation of document, with indication, where appropriate, of	the relevant passages	Relevant to claim No.			
 Х А	WO 00 65993 A (LANG BURRHUS ; (AT); LEONHARD LANG KG (AT)) 9 November 2000 (2000-11-09) page 3, line 29 -page 5, line	1-3,17, 19 5,6,10,				
	page 3, Time 23 page 4, Time	a , g	11, 14-16, 20-22, 27-31, 33,34, 37-40, 42-45			
		-/				
χ Fur	ther documents are listed in the continuation of box C.	X Patent family members are list	ed in annex.			
'A" docum	ategories of cited documents : ent defining the general state of the art which is not dered to be of particular relevance	or priority date and not in conflict w cited to understand the principle or	"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention			
filing : L* docum	document but published on or after the International date ent which may throw doubts on priority claim(s) or is cited to establish the publication date of another or other special reason (as specified) ent referring to an oral disclosure, use, exhibition or	"X" document of particular relevance; the cannot be considered novel or can involve an inventive step when the "Y" document of particular relevance; the cannot be considered to involve an document is combined with one or ments, such combination being ob-	not be considered to document is taken alone e claimed invention Inventive step when the more other such docu-			
citatio O' docum	means					
citatio 'O' docum other 'P' docum		in the art. "8" document member of the same pate				
citatio O" docum other P" docum later t	means ent published prior to the International filing date but	in the art.	nt family			
citatio O" docum other P" docum later t	means ent published prior to the International filing date but han the priority date claimed	in the art. "&" document member of the same pate	ent family search report			

INTERNATIONAL SEARCH REPORT

Int inal Application No PCT/US 02/17393

	ation) DOCUMENTS CONSIDERED TO BE RELEVANT	
Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X A	US 5 395 398 A (ROGOZINSKI WALLACE J) 7 March 1995 (1995-03-07) column 4, line 45 -column 5, line 54;	1,3,5-7, 9,10,14, 15, 17-19, 21-24, 26-32 2,11,13, 16,20,
	figures 	33,34, 36-45
A :	US 5 433 735 A (ZANAKIS MICHAEL F ET AL) 18 July 1995 (1995-07-18) cited in the application	1,3,5,6, 8,10,11, 15,16, 19-23, 25, 27-30, 33, 37-40, 42-45
	column 6, line 12 -column 7, line 60; figures 1-4 	
A	US 4 619 252 A (IBBOTT JACK K) 28 October 1986 (1986-10-28)	1,3-5,9, 10, 14-16, 19-22, 26,27, 29,30, 33,41-45
	column 3, line 16 -column 5, line 2; figures 	
A	US 5 853 424 A (RISE MARK T) 29 December 1998 (1998-12-29) column 1, line 27 -column 2, line 5 column 2, line 44 -column 4, line 55; figures	33
A	EP 0 947 214 A (BANGAHDO KK) 6 October 1999 (1999-10-06) page 3, column 4, line 28 -page 4, column 6, line 25; figures	33,37, 39,42-45
A	WO 98 26838 A (PARKER THEODORE L ;NICHOLIC SERJAN (US); VIDACARE INTERNATIONAL IN) 25 June 1998 (1998-06-25) page 4, line 7 -page 5, line 28; figures	1,4

FURTHER INFORMATION CONTINUED FROM PCT/ISA/ 210

This International Searching Authority found multiple (groups of) inventions in this international application, as follows:

1. Claims: 1-32

An electrode system for facilitating the healing of a wound, comprising: a support structure, a first electrode attached to the support structure and a second electrode attached to the support structure, wherein the second electrode surrounds the first electrode on the support structure, and wherein (a) when the electrode system is applied to the wound and (b) when the voltage potential is applied across the first and the second electrodes, a current is caused to flow between the first and the second electrodes, thereby passing through the wound.

2. Claims: 33-45

An electrode system for facilitating the healing of a wound, comprising: a first electrode and a second electrode, wherein the first and second electrodes comprise oppositely charged polymers of sufficient differential voltage potential and sufficient charge densities to cause a current to flow from the first electrode to the second electrode through the wound.

INTERNATIONAL SEARCH REPORT

formation on patent family members

Int nel Application No PCT/US 02/17393

	atent document d in search report		Publication date		Patent family member(s)		Publication date
WO	0065993	A	09-11-2000	AT AT WO CN EP JP	407486 76999 0065993 1353592 1173095 2002542866	A A1 T A1	26-03-2001 15-08-2000 09-11-2000 12-06-2002 23-01-2002 17-12-2002
US	5395398	Α	07-03-1995	NONE			
US	5433735	A	18-07-1995	NONE	· • • • • • • • • • • • • • • • • • • •		
US	4619252	A	28-10-1986	JP JP JP JP AU AU EP WO KR	1654089 3013910	B A C B A B2 A A1 A1	27-11-1992 20-12-1991 29-08-1985 13-04-1992 25-02-1991 05-11-1984 29-09-1988 07-11-1984 15-05-1985 25-10-1984 04-10-1991
US	5853424	Α	29-12-1998	NONE			
EP	0947214	Α	06-10-1999	EP	0947214	A2	06-10-1999
WO	9826838	Α	25-06-1998	AU WO	5711698 9826838		15-07-1998 25-06-1998

This Page is Inserted by IFW Indexing and Scanning Operations and is not part of the Official Record

BEST AVAILABLE IMAGES

Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images include but are not limited to the items checked:

□ BLACK BORDERS
□ IMAGE CUT OFF AT TOP, BOTTOM OR SIDES
□ FADED TEXT OR DRAWING
□ BLURRED OR ILLEGIBLE TEXT OR DRAWING
□ SKEWED/SLANTED IMAGES
□ COLOR OR BLACK AND WHITE PHOTOGRAPHS
□ GRAY SCALE DOCUMENTS
□ LINES OR MARKS ON ORIGINAL DOCUMENT
□ REFERENCE(S) OR EXHIBIT(S) SUBMITTED ARE POOR QUALITY
□ OTHER:

IMAGES ARE BEST AVAILABLE COPY.

As rescanning these documents will not correct the image problems checked, please do not report these problems to the IFW Image Problem Mailbox.